

Figure 3.1 (a)

Figure 3.1 (b)

Considering a second example, shown in **Figure 3.1 (b)**, of a base insulated, top loaded vertical radiator, it can be seen that the current then tapers to zero at the extremities of the capacity top hat. The average current flowing in the vertical section is clearly increased above that in the first example; hence, the effective height h_e is said to be increased.

In quantitative terms, the increase in h_e is dependent upon the relative values of the capacities of the mast and the top hat, such that the effective height, h_e is given by:

$$H_e = h \left[1 - \frac{1}{2} \left(\frac{C_M}{C_M + C_H} \right) \right]$$

Equation 7

Where:

- > h = actual height
- > C_M = capacity of vertical section
- > C_H = capacity of horizontal section

(See paragraph 3.2 to estimate the capacity of antenna sections).

Top loading is often achieved by the use of guys that are electrically connected to the top of the tower with insulators placed part way down their length. It is obvious that if these insulators are positioned close to the ground the top capacity will be increased but the average height of the top hat will be reduced. As a compromise, the insulators are usually placed at a vertical height above ground level equal to 4/7 of the height of the tower.

A third example may be considered in which the mast is grounded and an insulator is placed between the top of the mast and the capacity top hat. With this arrangement, the loading coil must also be positioned at the top of the mast. The total input current I then flows through the full height of the mast therefore $h_e = h$.

As shown in equations (1) and (2), the radiation resistance $R_R \propto h_e^2$ and efficiency $N \propto R_R$ (approximately).

Hence, efficiency $N \propto h_e^2$ (approximately).

It is, therefore, important to obtain as much effective height as possible which, in turn, is achieved by positioning the loading coil as high as possible on the antennas structure.

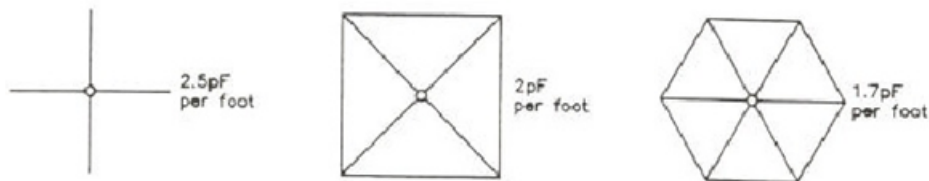
3.2 Antenna Capacity:

Increasing the antenna capacity increases the system bandwidth and efficiency by reducing the necessary value of loading coil inductance together with its series loss resistance.

Antenna capacities can be roughly estimated using the following data:

<u>Antenna</u>	<u>Approximate Capacitance Allowance</u>
Base-insulated vertical lattice tower	5 – 6pF per foot
Whip or other than vertical radiator	4pF per foot
Single horizontal or vertical wire	3pF per foot

Where more than a single wire is used, the effective capacity per foot is reduced by mutual coupling between the wires therefore they should be positioned as far apart as possible. Considering the plan view of the top loading umbrella perpendicular to the mast, the following capacitance can be estimated for the total length of the radiating elements.



When top loading guys are used, the capacity per foot is reduced because they do not lie in a single plane and the coupling between the guys and the vertical radiator is increased. Where four top loading guys at 45° to the mast are used, a capacity of 1.5pF per foot may be estimated.

3.3 Ground Loss Resistance

Calculation of the effective series loss resistance of particular ground mat configuration is rather complex and is not covered in detail here. Instead, examples of some commonly used arrangements using sets of radial conductors placed symmetrically around the antenna base are shown. These may be used as a guide to estimate the ground loss resistance for similar configurations.

<u>Number of Radials</u>	<u>Length of Radials</u>	<u>Ground Resistance (ohms) at Operating Frequency (Fo)</u>			
		<u>200kHz</u>	<u>300kHz</u>	<u>400kHz</u>	<u>500kHz</u>
6	165ft	15	8	6	5
18	500ft	4.5	4	3.5	3
120	1000ft	2.5	2	1	0.5

It should be emphasized that these values are approximate, being somewhat dependent upon the effective height of the associated antenna and the ground conductivity in the vicinity of the ground mat.

3.4 Antenna Loss Resistance

This resistance is usually quite small and can be ignored in all but the most efficient antennas. A figure of $R_a = 0.1$ ohm could be used as a rough approximation.

3.5 Sample Calculations of Antenna Characteristics

Consider a base insulated, 150ft lattice tower with umbrella top loading consisting of four radials each 50ft long. Its ground plane uses 24 x 500ft radials. The antenna is fed from a 1kW transmitter at 300kHz modulated at 1020Hz. Estimate the antenna reactance, effective height, radiation resistance, ground loss resistance, efficiency, bandwidth, sideband attenuation and peak voltage (assume a coil Q of 300).

3.5.1 Antenna Capacities:

Mast capacity $C_M = 6 \times 150 = 900\text{pF}$

Top hat capacity $C_H = 4 \times 50 \times 1.5 = 300\text{pF}$

Total capacity = 1200pF

$$\text{Antenna reactance } X_C = -j \left[\frac{1}{2\pi F C} \right] = -j \left[\frac{1}{2\pi \times 300 \times 10^3 \times 1200 \times 10^{-12}} \right]$$

$$X_C = -j 442 \text{ ohms}$$

The loading coil reactance must be $+j 442$. Assuming of coil Q factor of 300 the coil loss resistance

$$R_L = \frac{442}{300} = 1.47 \text{ ohm}$$

3.5.2 Radiation Resistance

From **Equation 7**

$$\begin{aligned} \text{Effective height } h_e &= h \left[1 - \frac{1}{2} \left(\frac{C}{C_M + C_H} \right) \right] \\ &= 150 \left[1 - \frac{1}{2} \left(\frac{900}{900 + 300} \right) \right] \\ h_e &= 93.75 \text{ ft.} \end{aligned}$$



$$\text{wavelength at 300kHz} = \frac{300 \times 10^6 \text{ m}}{300 \times 10^3} = 1000 \text{ m}$$

$$= 3280 \text{ ft}$$

from **Equation 1**

$$\text{Radiation resistance } R_R = 160 \times \pi^2 \times \left(\frac{93.75}{3280} \right)^2$$

$$R_R = 1.29 \text{ ohm}$$

3.5.3 Ground Loss Resistance:

From table in paragraph 3.3 the ground loss resistance will be less than 4 ohms, say 3.9 ohms.

3.5.4 Antenna Efficiency:

from **Equation 2**

$$\text{Antenna Efficiency } N = \frac{R_R}{R_R + R_L + R_A + R_G} \times 100\%$$

$$= \frac{1.29 \times 100\%}{1.29 + 1.47 + 0.1 + 3.9} = 19.1\%$$

$$\text{Hence, radiated carrier power} = 1 \text{ kW} \times \frac{19.1}{100} = 191 \text{ W}$$

$$\text{The radiated power} = I_A^2 \times R_R = 191 \text{ W}$$

From equation **Equation 4**

$$A_S = 10 \log_{10} \frac{1}{1 + Q_A^2 \times \left| \frac{2 F_M}{F_O} \right|^2} \text{ dB}$$

$$\text{Sideband Attenuation} = 10 \log \left| \frac{1}{1 + 65.38^2 \times \left| \frac{2040}{300 \times 10^3} \right|^2} \right| \text{ dB}$$

$$= 0.78 \text{ dB}$$

or mod depth is reduced by 8.6%

i.e. if mod depth were 95% at the input, the radiated mod depth would be $95 \times .914 = 86.8\%$.

Hence, effective modulation component of antenna current = $I_A \times .868$.

3.5.6 Peak Antenna Voltage:

At the peak of the modulation envelope the antenna voltage is given by

$$V_p = (I_A + .868 I_A) \sqrt{2} X_C$$

$$= 1.868 \times 12.16 \times \sqrt{2} \times 442 = \underline{14,196 \text{ V peak}}$$